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# MECHANICAL-PROPERTY DATA TD NICKEL

Stress-Relieved Sheet

Issued by

Air Force Materials Laboratory Research and Technology Division Air Force Systems Command Wright-Patterson Air Force Base, Ohio

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Prepared by

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AF 33(615)-2494

This data sheet was prepared by Battelle Memorial Institute under Contract AF 33 (615)-2494. The contract was initiated under Project No. 7381, "Materials Application", Task No. 738106, "Design Information Development". The major objectives of this program are to evaluate newly developed structural materials of potential Air Force weapons-system interest and then to provide data-sheet-type presentations of mechanical data. The program was assigned to the Structural Materials Engineering Division at Battelle under the supervision of Mr. Walter S. Hyler. Project engineer was Mr. Leman Beall, Jr.. The program was administered under the direction of the Air Force Materials Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, by Mr. Marvin Knight, project engineer.

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#### TD NICKEL

TD Nickel is a recently developed alloy containing 2 volume percent thoria and the balance nickel (Ni - 2ThO<sub>2</sub>). This alloy shows promise as a structural material for use in the temperature range from 1900 to 2400 F. It has excellent thermal stability, high thermal conductivity, and a high melting point.

The material has sufficient ductility for simple cold-forming operations and can be machined in the same manner as stainless steel.

Fusion welding requires special techniques to achieve sound joints. However, this alloy can be joined quite readily by brazing, ultrasonic welding, and diffusion bonding.

The alloy is available as sheet, bar, tubing, wire, foil, and forging.

## TD NICKEL SHEET DATA(a)

Condition: Stress-relieved(b)
Thickness: 0.060 inch

Properties	Temperature, F			
	RT	1600	1800	2000
Tensile				
F <sub>tu</sub> (longitudinal), ksi	63.6	21,4	17.9	14. 7
Ftu (transverse), ksi	63.8	20.6	17.1	13. 3
F <sub>ty</sub> (longitudinal), ksi	46. 2	21.2	17.7	14. 3
Ftv (transverse), ksi	45.6	20.3	16.8	12. 9
et (longitudinal), percent in 2 in.	14.5	5.0	5.0	8. 0
et (transverse), percent in 2 in.	14.5	3. 0	3. 0	3. 0
Et (longitudinal), psi x 106	16.9	10.7	9. 1	8. 2
Et (transverse), psi x 106	17.8	10. 3	8.8	8. 6
Compression				
F <sub>C</sub> y (longitudinal), ksi	42.1	20.9	17. 2	13.6
Fcy (transverse), ksi	49.4	20.3	16. 1	12.8
Ec (longitudinal), ksi	16.0	9.5	9. 9	7. 7
Ec (transverse), ksi	18.4	9. 7	9. 9	7. 4
Impact				
(V-notch Charpy) ft-1b(1)*	30	NA(c)	30	NA
Fracture Toughness	(d)	NA	NA	NA
Bend				
(Transverse)	Sharp(e)	NA	NA	NA

Properties	Temperature, F				
	RT	1600	1800	2000	
Shear, Fs			· · · · · · · · ·		
(Longitudinal), ksi	57.9	NA	NA	NA	
(Transverse), ksi	58. 4	NA	NA.	NA	
Axial Fatigue					
(Transverse)					
$10^3_{-}$ (K <sub>b</sub> = 1) (R = 0.1), ks:	63.0	23.0	19.0	NA	
$10^5 (K_t = 1) (R = 0.1), ksi$	<b>57.</b> 5	19.5	16.0	NA	
$10^7 (K_t = 1) (R = 0.1), ksi$	45.0	15.0	11.5	NA	
$10^{3}$ (Kt = 3) (R = 0.1), ksi	61.0	22.5	17. 0	NA	
$10^5 (K_t = 3) (R = 0.1), ksi$	3 <b>9. 0</b>	15.0	12.0	NA	
$10^7 (K_t = 3) (R = 0.1)$ , ksi	22. 5	10.0	8.0	NA	
Creep					
(Transverse)					
0.2% elongation 100 hr, ksi	NA	10.0	7.2	4.6	
0.2% elongation 1000 hr, ksi	NA	8.2	5. 2	3.5	
Stress Rupture					
Rupture 100 hr, ksi	NA	11.0	7.8	<b>5.4</b>	
Rupture 1000 hr, ksi	NA	9.0	5.8	4.4	
Stress Corrosion					
80 percent F <sub>ty</sub> 1000 hr max	No cracks(g) NA		NA	NA	
Coefficient of Thermal Expansion					
68 to 2000 F	$8.7 \times 10^6$ in. /in. /F				
Density (1,2)*	0.322 lb/in.3				
Ductile-to-Brittle Bend-Transition Temperature, F	Lower than -100 F(f)				

Melting Temperature

2650 F(3)

# 70 F = #00 (2,3) 500 F = 380 Notest Thermal conductivity, Btu/h2/in./hr/1°F 1100 F = 300 1500 F = 320 1700 F = 340 Electrical registivity, migrehm-em (70 F) 7.6 (2,3) Specific host, Bru/16/0F 0.106 (2,3)

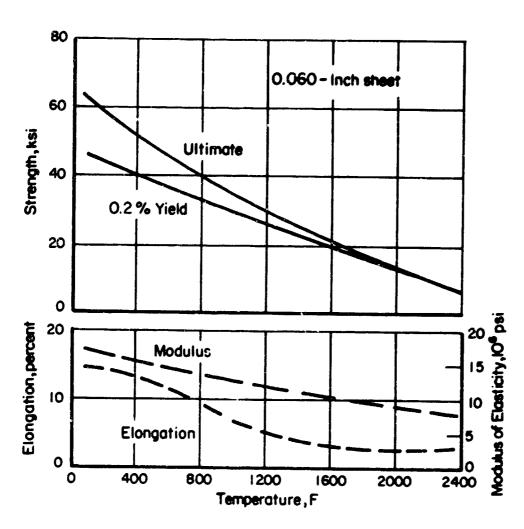
<sup>(</sup>b) Treatment: 1 hr. at 2000 F in hydrogen. Test material from two production heats.

<sup>(</sup>c) Information either not evallable or not applicable.

<sup>(</sup>d) Fatigue-cracked center-notched specimens (0.060 x  $3^{\circ}$  x  $12^{\circ}$ ) failed in a ductile man

<sup>(</sup>a) Sharp bending Tup (75-dag angle); specimen unloaded band ungle over 100 dag; no crecks at RT.

<sup>(</sup>f) Sharp bonding Tup (75-dag angle); no cracks at -100 F.
(g) Alternate immersion 2% % NeCL.



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FIGURE 1. EFFECT OF TEMPERATURE ON THE TENSILE PROPERTIES OF STRESS-RELIEVED TD NICKEL SHEET

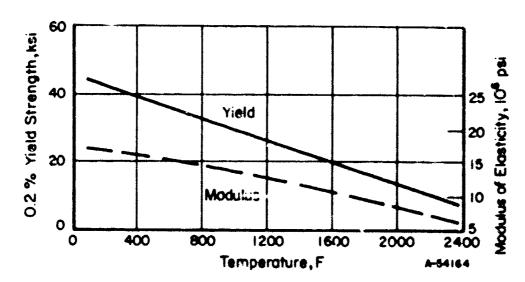


FIGURE 2. EFFECT OF TEMPERATURE ON THE COMPRESSION PROPERTIES OF STRESS-RELIEVED TD NICKEL SHEET

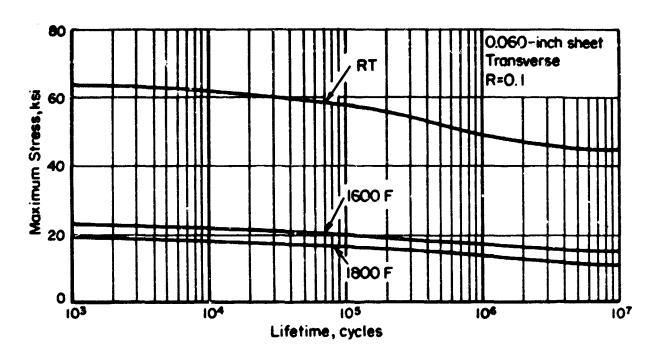


FIGURE 3. AXIAL-LOAD FATIGUE RESULTS FOR STRESS-RELIEVED TO NICKEL SHEET AT THREE TEMPERATURES

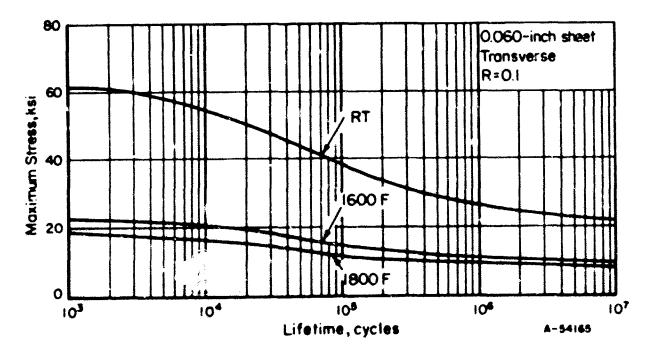


FIGURE 4. AXIAL-LOAD FATIGUE RESULTS FOR NOTCHED (K<sub>t</sub> = 3.0), STRESS-RELIEVED TD NICKEL SHEET AT THREE TEMPERATURES

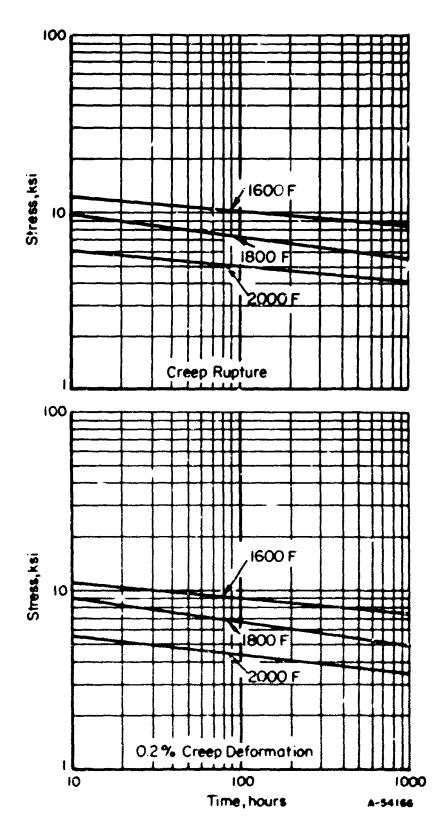


FIGURE 5. STRESS-RUPTURE AND 0, 2% DEFORMATION CURVES FOR TD NICKEL SHEET (0, 060 INCH) AT THREE TEMPERATURES

#### REFERENCES

- (1) Anders, F. J., Jr., Alexander, G. B., and Wartel, W. S., "A Dispersion-Strengthened Nickel Alloy", Metal Prog., 82 (6), 88-91, 118-122 (December, 1962).
- (2) "TD Nickel Dispersion Strengthened Nickel", Report A-41076, Du Pont Metal Products Product Information, undated.
- (3) Stuart, R. E., and Starr, C. D., "New Design Data on TD Nickel", Mater. Design Eng., 58 (2), 81-85 (August, 1963).

crossed interferometers
fundamental and hermonic frequency
asymmetric gases
methylene chloride, methylene fluoride, and
difluoroethylene
coaxial tunable magnetron
beam splitters

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